Non-Destructive Evaluation of Polymer Coating Structures on Pharmaceutical Pellets Using Full-Field Optical Coherence Tomography

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Received 16 September 2013; revised 8 October 2013; accepted 10 October 2013
Published online 1 November 2013 in Wiley Online Library (wileyonlinelibrary.com). DOI 10.1002/jps.23764

ABSTRACT: Full-field optical coherence tomography (FF-OCT) using a conventional light-emitting diode and a complementary metal-oxide semiconductor camera has been developed for characterising coatings on small pellet samples. A set of en-face images covering an area of 700 × 700 μm² was taken over a depth range of 166 μm. The three-dimensional structural information, such as the coating thickness and uniformity, was subsequently obtained by analysis of the recorded en-face images. Drug-loaded pharmaceutical sustained-release pellets with two coating layers and of a sub-millimetre diameter were studied to demonstrate the usefulness of the developed system. We have shown that both coatings can be clearly resolved and the thickness was determined to be 40 and 50 μm for the outer and inner coating layers, respectively. It was also found that the outer coating layer is relatively uniform, whereas the inner coating layer has many particle-like features. X-ray computed microtomography measurements carried out on the same pellet sample confirmed all these findings. The presented FF-OCT approach is inexpensive and has better spatial resolution compared with other non-destructive analysis techniques such as terahertz pulsed imaging, and is thus considered advantageous for the quantitative analysis of thin coatings on small pellet samples.

INTRODUCTION

An ever increasing number of modified release technologies are available to the pharmaceutical industry for the purpose of improving drug therapy via oral administration.1 Small-sized pellets of sub-millimetre diameter have been used to control the release rate of active pharmaceutical ingredients (APIs) in the human body. They are designed to be coated and filled into capsules or compressed into other solid dosage form. The use of pellets allows a more even spread of drug after the dissolution of capsule shell and thus ensures the drug absorption within gastrointestinal tract2 as well as avoiding dose-dumping problems because of local defects in the coating structure which are much more severe in a monolith as opposed to a multi-particulate release system. Depending on the required dissolution profile, the API can be contained in the pellet core, or directly coated onto a core bead typically made of sugar or polymer excipients. By using sophisticated coatings such as enteric coatings and complex layer structures applied on pellets, it is possible to direct and extend the release time to attain full therapeutic efficiency. As the coating quality has a direct impact on the therapeutic efficiency, there is a critical need for analytical techniques to non-destructively assess the coating structures on pharmaceutical pellets.

The current quality control procedures during film coating processing generally evaluate the coating quality of pellets in terms of the average weight gain.3 The measurement is non-specific and the weight gain may fail to reflect the coating structure of the sample.4 Investigation into the physical characteristics of pellets is commonly undertaken with microscopy techniques. Images are generally recorded from cross-section cuts of pellets, and coating thicknesses are evaluated by measuring the distance between manually marked points on the coating borders.5 However, this method is very time consuming, it is destructive and can induce artefacts because of plastic deformation during the preparation of cross-sections.6

Near infrared (NIR) spectroscopy, which is a non-destructive method, has long been used to evaluate pellet coatings in the pharmaceutical industry. However, NIR spectroscopy is inherently an indirect method as it needs additional reference techniques to build a calibration model.7 Terahertz pulsed imaging (TPI) has also been demonstrated as a powerful method for the non-destructive evaluation of coatings on large pharmaceutical tablet.8–10 It is an excellent technique to study the coating structure of relatively large pharmaceutical tablets because of its high penetration depth. For small pellets such as the ones studied here which make up the bulk of pharmaceutically used pellets, however, TPI cannot comprehensively resolve the layer structures because of its inherently low lateral resolution, which is fundamentally limited by the relatively large wavelength of terahertz radiation (e.g., 300 μm at 1 THz), thus leading to strong scattering from sub-millimetre size pellets.

Recently, we and other groups have demonstrated that optical coherence tomography (OCT) can be used for characterising the coating thickness of pharmaceutical tablets11,12 and for imaging pharmaceutical tablets.13 Tablet coatings with a layer thickness range of 10–60 μm were measured quantitatively.11 In all these studies, single-point frequency domain OCT systems were used where the depth profile (A-scan) at a given
transverse location was obtained using a focused probe beam from a broadband light source. A succession of these A-scans along one dimension of the transverse plane provides a two-dimensional cross-section map (B-scan). A full three-dimensional volume is obtained by collecting successive B-scans. Therefore, a full OCT measurement requires electromechanically scanning either the sample or the OCT optics in two lateral dimensions. For small pellet samples, however, this approach proves to be difficult and inefficient to perform OCT measurements because of the small size (pellet diameter is less than 1 mm).

In this work, we report the development of a full-field OCT (FF-OCT) system for characterising small size pellets. Our FF-OCT system uses an inexpensive conventional infrared light-emitting diode (LED) as the broadband light source and a complementary metal-oxide semiconductor (CMOS) camera as the detector. The measurement is done in parallel. The sample is full-field illuminated and en-face imaged with the CMOS camera, hence eliminating the need for an electromechanical lateral scan. We demonstrate that small-sized pharmaceutical pellets can be imaged easily using the presented FF-OCT system, with a high-spatial resolution of 3.6 and 11 μm in axial and lateral directions, respectively.

**EXPERIMENTAL**

**FF-OCT Imaging Setup**

Figure 1 shows the schematic diagram of a table-top FF-OCT system which was based on a Michelson interferometer. Broadband light from a conventional infrared LED source (λ₀ = 850 nm, Δλ = 90 nm) was first split into reference and sample arms by a non-polarising 50/50 beam-splitter. Light back scattered by the sample was recombined with the light reflected off the reference mirror at the beam splitter and finally captured with a Firefly MV CMOS camera (Point Grey Research Inc, Richmond, British Columbia, Canada). Interference would occur when the optical path length difference between the reference and sample arms is within the coherence length of the light source.

For a full OCT measurement, a series of en-face images was acquired at a rate of 120 frames per second while the reference mirror on a motorised stage was moving at a constant speed of 3 μm/s. This resulted in a fixed 25 nm depth interval between successive en-face images. Each en-face image is composed of 180 × 180 pixels (about 4 × 4 μm² per pixel) covering a sample area of 700 × 700 μm². The stage was scanned over a depth of 166 μm, thus the system eventually acquired a full OCT data cube covering a volume of 700 × 700 × 166 μm³.

**X-Ray Computed Microtomography**

The same pellet sample was analysed using a SkyScan1172 high-resolution X-ray computed microtomography (µCT) scanner (Bruker-microCT, Kontich, Antwerp, Belgium). The sample was imaged at an isotropic voxel resolution of 1.2 μm over a total of 5 h acquisition time and a subsequent image reconstruction time of about 4 h, using the NRecon program (version 1.6.8.0, Bruker-microCT).

The sample used in the presented work was a pellet with two coating layers. The core is a microcrystalline cellulose (MCC) sphere (Celphere MCC seed core CP-507, Asahi Kasei Corp., Tokyo, Japan). The inner coating layer is a drug-loaded layer containing 10% API and 90% hydroxypropyl methylcellulose (HPMC). The outer coating formulation contains a combination of ethyl cellulose and hydroxypropyl cellulose. As shown in the inset of the Figure 1, the coated pellet is approximately spherical with an outer diameter of about 850 μm.

**RESULTS**

Figure 2a shows a typical raw interferogram signal which is extracted from the volumetric OCT data cube recorded for a coated pellet sample. The tomography signal (Fig. 2b), which is a more intuitive and better representation of the sample depth profile, is calculated by demodulating the raw interferogram signal using a Hilbert Transform. A mean refractive index of 1.5 was used in all calculations. Several interference patterns are clearly visible. The first major interference feature at z = 0 corresponds to the reflection/scattering from the pellet surface. The full width at half maximum (FWHM) of the envelope of this main interferogram feature, which corresponds to the axial resolution achieved here, is determined to be 3.6 μm, as shown in the inset of Figure 3a. Note that the axial resolution of an OCT system is ultimately determined by the coherence length of the light source and can be calculated using the following equation:

\[
l_c = 0.44 \frac{\lambda_0^2}{\Delta \lambda}
\]

where λ₀ = 850 nm is the centre wavelength and Δλ = 90 nm is the spectral bandwidth of the LED light source used in our experiment. The axial resolution is thus theoretically calculated to be 3.5 μm which agrees very well with the measured resolution of 3.6 μm.

A set of cross-sectional images (B-scan images) was reconstructed from the recorded volumetric OCT data cube. Figure 3a shows one such B-scan image of the pellet sample, revealing its internal structures. A scale bar calibrated in decibel units is included. Black corresponds to the highest signal and white corresponds to the lowest. As shown in Figure 3a, two
A typical raw interferogram signal acquired from a two-layer pellet (a), and its corresponding tomography signal in decibel (b). The inset of Figure 2 (a) shows an enlarged view of the first main peak, with the envelope (in red) showing the demodulated tomography signal. The achieved axial resolution is 3.6 µm.

In (a), two dashed yellow lines were used to indicate the interfaces. The red arrows mark the position of the five signal traces plotted in Figure 4 (a). For comparison, both B-scan maps cover approximately an area of 700 × 166 µm² (lateral × axial). Note that the images do not correspond to the exact same location in each sample but are representative of the morphology in each case.

Figure 2. A typical B-scan map (cross-sectional image) of a pellet sample obtained non-destructively using FF-OCT (a) and XµCT (b). In (a), two dashed yellow lines were used to indicate the interfaces. The region of interest (ROI) is illustrated in Figure 5a. About 200 neighbouring OCT signals from this region (here of a diameter of 68 µm) were used to calculate a mean tomography signal. The area is chosen to provide sufficient number of tomography signals whilst the measurement error introduced by the surface curvature is still within an acceptable range (e.g., the thickness error is smaller than 0.2 µm for a 40-µm thick coating layer, referred to Figure 5b). Figure 4a shows five randomly selected tomography signals within this region, confirming that particle-like features or air bubbles appear randomly distributed in the range of approximately 41–90 µm. Figure 4b shows the mean tomography signal over the ROI by averaging all 200 OCT signals. As shown in this figure, the tomography signal in the range of approximately 41–90 µm has non-zero values, and its medium value was subsequently used to determine the starting and the end position of the inner coating layer (e.g., at a depth of 41 and 90 µm, respectively, as indicated by the two red dots.). Consequently, the mean coating thickness can now be easily determined to be 40 and 50 µm for the outer and inner coating layers, respectively.

It should be pointed out that for samples with uneven structures, such as the drug-loaded layer in the pellet sample studied in this work, the proposed method can be used for calculating the mean coating thickness, although it is not possible to obtain a coating thickness map of the sample. For tablets with coating layers were distinguishable (two yellow dashed lines were used to indicate the interface): the outer layer has a mean thickness of about 40 µm, whereas the inner layer has a mean thickness of 50 µm. In addition, Figures 2b and 3a also show that the first 40 µm thick layer is relatively “clean”, that is, no peaks in the tomography signal and no particle-like features in the B-scan image in the first 40 µm below the surface, indicating that the outer coating layer is fairly uniform. In contrast, the region of 41–90 µm below the pellet surface is dominated by multiple peaks in the tomography signal and particle-like features in the B-scan image, suggesting that the inner coating layer is not uniform at all. The particle-like features could be API particles that are dispersed in a HPMC matrix. Note that the presence of air bubbles in the coating layer could also lead to the particle-like features observed here. Thus further studies are needed to understand this this fully.

In order to validate the OCT results, we performed the XµCT measurement on the same pellet. Figure 3b shows the resultant XµCT B-scan image, confirming that the pellet sample indeed has two coating layers and the inner coating layer has many particle-like features with a transversal size of approximately 9 µm. The mean thickness of each layer was manually determined as the averaged thickness of 40 selected points from the B-scan map, and the obtained values were 40 and 50 µm, for the outer and inner coating layer, respectively. We can conclude that the FF-OCT results are consistent with those of XµCT.

One of the key metrics to characterise the coating structure of the pellet is the mean thickness of the respective coating layers. We note that for this specific type of pellet the boundary between neighbouring coating layers is not always clearly visible in the B-scan map (Fig. 3a), or in the optical microscope images (inset of Fig. 1). As further illustrated in Figure 4a, the coating thickness cannot be precisely determined from a single OCT signal. To determine the coating thickness in a robust and automatic way, we propose here to use the mean OCT signal over a wide central volume to calculate the coating thickness. The region of interest (ROI) is illustrated in Figure 5a. About 200 neighbouring OCT signals from this region (here of a diameter of 68 µm) were used to calculate a mean tomography signal. The area is chosen to provide sufficient number of tomography signals whilst the measurement error introduced by the surface curvature is still within an acceptable range (e.g., the thickness error is smaller than 0.2 µm for a 40-µm thick coating layer, referred to Figure 5b). Figure 4a shows five randomly selected tomography signals within this region, confirming that particle-like features or air bubbles appear randomly distributed in the range of approximately 41–90 µm. Figure 4b shows the mean tomography signal over the ROI by averaging all 200 OCT signals. As shown in this figure, the tomography signal in the range of approximately 41–90 µm has non-zero values, and its medium value was subsequently used to determine the starting and the end position of the inner coating layer (e.g., at a depth of 41 and 90 µm, respectively, as indicated by the two red dots.). Consequently, the mean coating thickness can now be easily determined to be 40 and 50 µm for the outer and inner coating layers, respectively.
uniform coating and core structures, the measured OCT signals show distinct peaks and the resultant B-scan maps show uniform coatings with clear boundaries, as reported in previous studies.

These distinct peaks correspond to the change in refractive index at the air/surface and coating/core interface of a tablet sample. Consequently, the coating thickness at each pixel (rather than the mean coating thickness) can be directly determined as the peak position difference (divided by the refractive index of the coating), in a similar way as in the coating analysis by using TPI. This allows the coating thickness map to be subsequently constructed as well. We can conclude that FF-OCT can be used to quantify the coating layer thickness and for characterising the uniformity of the coating layer.

As a further illustration of the microstructure of the pellet, Figure 6a shows a set of en-face images at progressive depths reconstructed for the pellet sample. Again the dark areas correspond to the region where there is a change in the refractive index, for example at the interface between two coatings or between two different materials (particle). Because of the surface curvature of the spherical pellet sample, one can see clearly the annular shape (in dark) in image A to F. In image G, a dark dot reappeared at the centre, indicating the inner coating layer starts to appear. The thickness of outer coating layer could then be estimated as 40 μm (image A–G). In a similar manner, the thickness of the inner coating layer could also be estimated as 47 μm (image G–N). As a comparison, Figure 6b displays seven XuCT en-face images of the same pellet sample at corresponding depths. Again there is a general agreement between the FF-OCT and the XuCT results.

Both Figures 3a, 3b) and 6a revealed that there are particle-like features within the inner coating layer and that these features have a wide range of particle size. To characterise the achieved lateral resolution of the developed FF-OCT system, a calibration specimen (stage micrometre, R1L382P, Thorlabs) was measured under the same experimental settings. Figure 7 shows the extracted surface height profile. The FWHM of the scale bar was measured to be 12 μm. The true width of the scale bar is about 5 μm as revealed by a more precise measurement using a high-resolution optical microscope. The lateral resolution of the presented OCT system, defined as the point spread function, is finally calculated as 11 μm through a deconvolution process.

We note that Pygall et al. and Laksmana et al. evaluated pellet coatings using confocal laser scanning microscopy (CLSM), which is a single-point imaging technique with depth selectivity. Both CLSM and OCT can provide high-resolution cross-sectional images of a sample. As a conventional microscope technique, CLSM detects the variation of optical intensity of the reflected/scattered light, whereas OCT detects the interference patterns (e.g., the electric field of the light reflected/scattered from the reference and sample arms). Thus OCT has a better imaging depth and is more sensitive to small changes in the inner structures/properties of a sample.

Terahertz imaging has also been evaluated for directly measuring the layer thickness of film coatings. As most pharmaceutical excipients used in film coating are either transparent or semi-transparent in the terahertz frequency range, TPI can be used to quantify thick pharmaceutical coatings in the range of 40–140 μm and beyond. However, because of the relatively long wavelength of terahertz radiation (300 μm at 1 THz), TPI has limited spatial resolution in lateral direction and thus is not suitable to investigate the fine structure of small-sized pellet samples such as the ones studied here. In contrast, the FF-OCT system presented in this study achieved a spatial resolution of 11 μm (lateral x axial) allowing a more precise analysis of the coating thickness and revealing more detailed information on the inner structures of a sample.
This makes the FF-OCT an attractive tool for non-destructive evaluation of small pharmaceutical pellets. We also demonstrated in this work that XμCT has excellent capability in obtaining the high-resolution three-dimensional inner structure of a pellet sample non-destructively. However, currently the XμCT measurement and the required subsequent image reconstruction is a time-consuming process (both on the order of hours for the XμCT results presented here). Furthermore, the ionising nature of X-ray radiation also makes it extremely difficult, if not impossible, to be used for online monitoring applications. In this sense, the FF-OCT method proposed here is advantageous as it is fast, compact and safe (it uses low power NIR light); thus, it could be used for both offline and online applications.

CONCLUSIONS

In this study, we have demonstrated the capability of FF-OCT for non-destructive evaluation of film coatings applied to spherical pellet of less than 1 mm diameter. By utilising the axial resolution of 3.6 μm, the layer thickness could be precisely determined as 40 and 50 μm for the outer and inner coatings of the pellet sample, respectively. The achieved lateral resolution is 11 μm and this allows particle-like features within the inner coating layer to be resolved. This, together with its low cost and ease of use, makes the presented FF-OCT an attractive analytical tool for the non-destructive evaluation of the coating thickness and internal structure of pharmaceutical pellets.
Figure 7. Surface height profile of two scale marks with a resolved FWHM of 12 µm. The inset shows the surface height image of the stage micrometre.

ACKNOWLEDGMENTS

This work is partially supported by the Engineering and Physical Sciences Research Council (EPSRC, EP/K031511/1). The authors would like to acknowledge Neil Turnbull from Pfizer UK for supplying samples of coated pellets used in this work.

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